

# **Reasons for FABER** Why maintaining the status quo is limiting us

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### The practical example of disproportions between research outcome and its implementation in engineering is prepared on the topic of multiaxial fatigue strength criteria

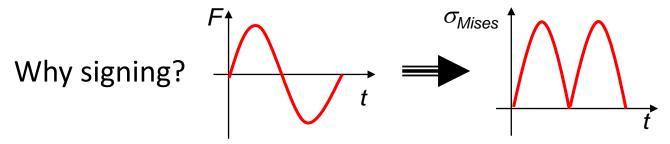
#### Multiaxial fatigue problem

- If more load channels interact, a phase shift among their periodical loadings can occur
- The non-zero phase shift between them can improve the fatigue properties (the maximums of the load are not concurrent)
- Also the combination of one static and one variable load channels – the common stress tensor reduction hypotheses fail

#### One of the Simplest Solutions

#### Signed von Mises stress

Can be used also for loading with non-constant amplitude



$$\sigma(t) = \sqrt{\frac{1}{2} \left[ \left( \sigma_x - \sigma_y \right)^2 + \left( \sigma_y - \sigma_z \right)^2 + \left( \sigma_z - \sigma_x \right)^2 + 6 \left( \tau_{xy}^2 + \tau_{yz}^2 + \tau_{zx}^2 \right) \right]}$$

PragTic 
$$\sigma^*(t) = \sigma(t) \cdot sign(I_1(t))$$
  
MSC.Nastran  
(and PragTic)  $\sigma^*(t) = \sigma(t) \cdot sign(max(|\sigma_1|, |\sigma_3|)) \longrightarrow \sigma_m^a \longrightarrow Walker$ 

### Criteria for Fatigue Limit Estimation

#### How to check them?

All fatigue criteria converted to the standard:

 $\begin{array}{c} D_p \leq f_{-1} \\ f_{-1} \end{array} \stackrel{D_p - \text{damage parameter} \sim \text{local stresses}}{f_{-1} - \text{fatigue limit in fully reversed axial loading}} \end{array}$ 

For an experimentally set multiaxial fatigue limit:

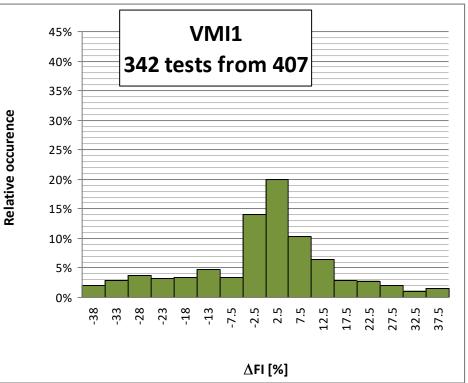
$$D_p = f_{-1}$$

Fatigue index error:

$$\Delta FI = \left(\frac{D_P - f_{-1}}{f_{-1}}\right) \cdot 100\%$$

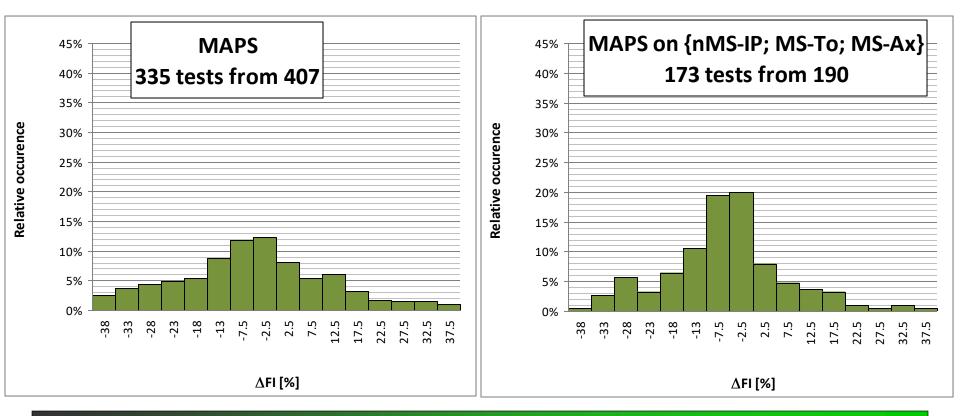
### ...But the Results...

- Signed von Mises
  - The difference between both signing variants is negligible overall
  - Optimum variant only for ductile materials and in-phase loading with zero mean stress
  - Problems
    - Mean axial stress within multiaxial loading
    - Mean torsion stress within multiaxial loading



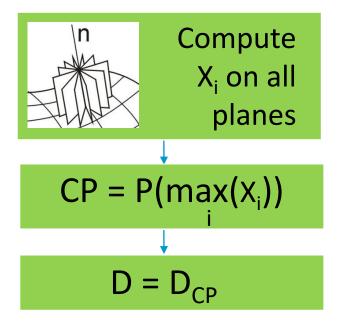
### MSC.Fatigue - MAPS

- Maximum Absolute Principal Stress
- Provides the best overall results, though they are not very good



# Multiaxial fatigue assessment criteria

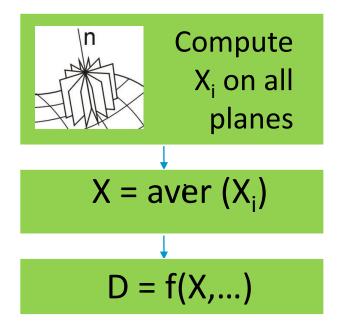
#### **Critical plane methods**



Mc Diarmid, Wang & Brown, Dang Van

- Critical plane according to:
  - Maximum Shear Stress/Strain Range (MSSR)
  - Maximum Damage (MD)
  - Critical Plane Deviation (CPD)
  - other...

#### **Integral methods**



Papadopoulos, Kenmeugne et al.

- Averaging ~ Integration
- Integrate:
  - Complete damage parameter
  - Individual variables

### Solutions for fatigue limit estimation today

#### In fatigue solvers:

Commercial									No	on-co	mmer	cial	Test set 407 exps.			
Methods	Fe-Safe	MSC.Fatigue	Femfat	FEARCE	nCode DesignLife	LMS Virtual. Lab Durability	WinLife		eFatigue	Code Aster	PragTic	FatLab	Mean relative error [%]	St. deviation of relative error [%]		
Dang Van (1973)	Х	Х		Х	Х	Х	X		X	X	X		-0.1	12.2		
Findley (1957)							Х		Х		Х	Х	8.7	15.2		
McDiarmid (1991)		Х		Х	Х						Х		-6.2	12.0		
Sines (1959)									Х		Х		-4.3	17.9		
Matake (1977)										Х	Х		6.4	15.8		
Other solution			Х							Х	Х	Х				

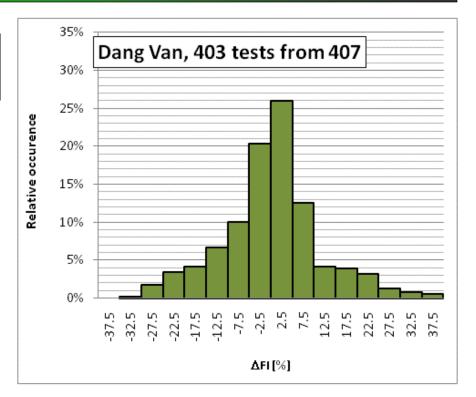
•  $\Delta$ FI – relative error between predicted and experimental fatigue limit

- $\Delta$ FI =0 ideal
- ▲FI >0 conservative
- $\Delta$ Fl <0 non-conservative

### Dang Van criterion

$$a_{DV} \cdot C_a + b_{DV} \cdot \sigma_{H,\max} \leq f_{-1}$$

- Critical plane criterion
- The most often used representative of multiaxial criteria
- Use of maximum hydrostatic stress does not seem to give acceptable results
- C: MS, Ax+Ax
- N-C:
  - nMS, OP
  - MS,To



average: -0.1%

range: 92.9%

standard deviation: 12.2%

### Weakness of Dang Van method

#### Hard to believe: multiaxial fatigue

			relative difference between predicted
Mean values of $\Delta FI$ in individual groups (tests)	CRO	DV	and experimental fatigue limit
All (407)	-8.0	-0.1	
nMS (171)	-3.1 -11.5	-0.6 -7.9 ×	no mean stress, out-of-phase loading
nMS,OP (40) nMS,IP (131)	-11.5	1.7 <	
marsin (191)	-0.5	1.7	no mean stress, in-phase loading

 There is a significant difference in mean prediction values depending on the phase shift of individual load channels

# Fatigue limit solution today

In		Meth	od:		C&S	Crossland	Dang Van	Findley	Fogue	Goncalves	L&M	L&Z	Matake	McDiarmid	Papadopoulos	Papuga PCr	Robert	Sines	Susmel
research					E.	9	3	L-	5	5	5	6	2				×	6	7
papers:	Ye Ref	ear of pu Year 1997	Sets	on: Items 43	2001	X 1956	1973	1957	1987	2005	2005	1989	X 1977	X 1991	X 1994	2008	1988	X 1959	2001
Well, the software		1999 2000 2001	4 1 ? 3	2 179 30	А	X X	Х	X				А	X X	x X	Х			Α	
developers cou try also Liu & Mahadevan ar		2002 2003 2005 2006 2007	52 3 4 1 16	447 38 41 8 125	X	X X	X X	х		А		Х		X	X X X X				А
maybe should dare to		2007 2008 2009 2010 2010	4 40 13 6	43 320 131 66	л	X X X X	X						X X	X	X X X	Х		X	х
implement Crossland in order to keep t	the	2010 2011 2011 2013 2014	49 8 8 2	407 52 62 4	$\mathbf{X}^*$ A	X* X* X X X	X* X*	X* X*	X* X*	X* X*	X*	X* X*	X* X*	х Х* Х*	X* X*	A*	X* X*	X* X* X X X	X*
prediction as b as now		2014 2014 2014 2015 2015	18 3 25 7	58 ? 269 26	А	X	Х	X X X		Х			X	Х	X X X			X	
	Mea	nber of c un relativ lev. of re	e erroi	ences [%]	2 -4.8 8.7	13 -8.0 11.3	7 -0.1 12.2	7 8.7 15.2	2 2.4 10.8	3 0.7 10.9	1 -1.2 12.1	3 0.0 8.8	7 6.4 15.8	7 -6.2 12.0	14 -4.6 10.3	1 -0.5 6.1	2 4.7 9.9	7 -4.3 17.9	2 1.7 8.4

#### Manson-McKnight

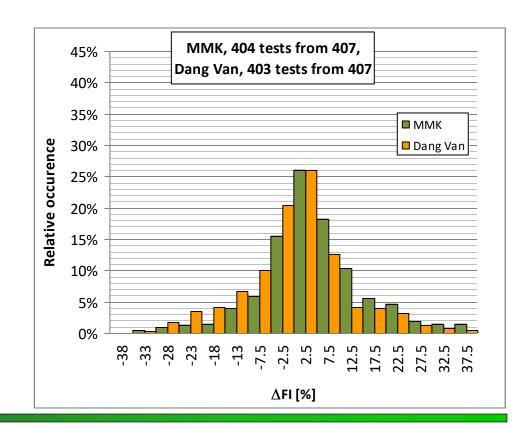
- So simple, that it can be computed in MS Excel
  - IThe cycle has to be detected a priori!
- Amplitude and mean value of each stress component is evaluated:

$$\sigma_{a} = \sqrt{\frac{1}{2} \left[ (\sigma_{x,a} - \sigma_{y,a})^{2} + (\sigma_{y,a} - \sigma_{z,a})^{2} + (\sigma_{z,a} - \sigma_{x,a})^{2} + 6(\tau_{xy,a}^{2} + \tau_{yz,a}^{2} + \tau_{zx,a}^{2}) \right]}$$
  
$$\sigma_{m}^{*} = sign[I_{1,d}] \cdot \sqrt{\frac{1}{2} \left[ (\sigma_{x,m} - \sigma_{y,m})^{2} + (\sigma_{y,m} - \sigma_{z,m})^{2} + (\sigma_{z,m} - \sigma_{x,m})^{2} + 6(\tau_{xy,m}^{2} + \tau_{yz,m}^{2} + \tau_{zx,m}^{2}) \right]}$$

 The mean equivalent value is signed according to the stress tensor invariant with biggest magnitude

#### Manson-McKnight - Results

- Not that bad
- Shift to conservative prediction results in many cases (To; nMS-OP; Ax+To; brittle materials)
- Ax+Ax with a phase shift – unsafely nonconservative (mean value △FI=-17.2%)
- In many other groups
   Dang Van better, but
   fails in MS cases



# MMK versus Dang Van

DV – Dang Van critical plane method (1974) MMKF – Manson-McKnight according to Filippini (2010)

MMK not to be	$\Delta {\rm FI}$ in individual groups	M	ean valu	es		Range		Stand	lard devia	ation
	(tests)	DV	MMKF	Diff	DV	MMKF	Diff	DV	MMKF	Diff
used for	All (407)	0	1	1	93	106	13	12	12	-1
	nMS (171)	-1	5	5	53	71	18	8	9	1
brittle materials	nMS,OP (40)	-8	8	16	53	70	18	12	14	2
	nMS,IP (131)	2	4	2	22	45	22	4	7	3
<ul> <li>MS,Ax+Ax,</li> </ul>	MS (236)	0	-1	-2	93	82	-11	15	12	-2
	MS,Ax (41)	-1	0	1	64	62	-2	13	11	-2
PS<>0	MS,To (18)	-16	-5	11	46	65	19	12	16	4
out-of-phase	MS,Ax+Ax (36)	12	-11	-23	57	43	-14	13	12	-1
- Out-or-phase	MS,Ax+Ax,noPS (18)	15	-3	-18	43	22	-20	12	8	-4
loading	MS,Ax+Ax, PS<>0 (18)	9	-19	-28	57	40	-18	14	10	-4
8	Ax+To (285)	-2	3	5	63	96	33	10	10	0
MMK useful for	MS,Ax+To (114)	-3	0	3	61	66	5	12	10	-1
	MS-Ax, Ax+To (52)	-1	6	7	61	43	-18	12	9	-4
pressure vessels	MS-To, Ax+To (31)	-10	-6	3	41	41	1	9	8	-1
•	ductile (352)	0	0	0	93	82	-11	13	11	-2
MS,Ax+Ax,noPS	ductile,nMS (118)	-1	4		43	30	-12	8	5	-3
	ductile,nMS,IP (86)	3	3	1	18	18	1	4	5	1
The difference is	brittle (37)	-1	11	12	42	75	33	7	16	9
	brittle, nMS(35)	-1	12	13	42	70	27	7	16	9
not big overall!	brittle,nMS,IP (29)	-2	8	10	16	44	28	3	11	8
Č	extra-ductile (18)	2	0	-2	19	18	-1	5	4	-1
	extra-ductile,nMS,IP (16)	3	-1	-4	12	11	-2	3	3	0

# Versions of Papuga PCr solution

- PCr original solution (2008) presented in IJF
- PCrN new version (2019) including mean shear stress effect
- New special formula includes both N<sub>m</sub> and C<sub>m</sub> mean stress parameters – a part of the N<sub>m</sub> effect moved to C<sub>m</sub> effect
- It improves mean value of MS,To group
- Substantially improves scatter by MS,Ax and MS,Ax+Ax experiments!
- Minor worsening in MS-Ax,Ax+To group – a further study will be done before a final publishing

$\Delta$ FI in individual groups	M	lean val	ues		Rar	nge		Standard deviation			
(tests)	DV	MMKF				iff		/MKF	Diff		
All (407)	0	)	1	1	93	106	13	12	12	-1	
ΔFI in individual gr	ouns	Mea	an val	ues		Range		St	tandar	rd	
(tests)	oups	PCr	PCrN	Diff	PCr	PCrN	Diff	PCr	PCrN	Diff	
All (407)		-1	1	2	37	31	-6	6	5	-1	
nMS (171)		1	1	0	23	23	0	4	4	0	
nMS,OP (40)		0	0	0	23	23	0	6	6	0	
nMS,IP (131)		1	1	0	17	16	0	3	3	0	
MS (236)		-1	2	3	37	31	-6	7	6	-2	
MS,Ax (41)		-2	2		33	24	-9	7	5	-2	
MS,To (18)		-8	-2	7	17	16	0	5	4	-1	
MS,Ax+Ax (36)		-4	4		32	20	-12	7	5	-2 -2 -3	
MS,Ax+Ax,noPS (18)		-4	4		25	19	-5	8	6	-2	
MS,Ax+Ax, PS<>0 (18	)	-4	4	8	27	15	-11	7	4	-3	
Ax+To (285)		1	1	1	36	31	-4	5	5	0	
MS,Ax+To (114)		1	2	1	36	31	-4	6	6	0	
MS-Ax, Ax+To (52)		0	3	3	28	31	3	6	6	0	
MS-To, Ax+To (31)		3	3	0	24	19	-5	5	5	0	
ductile (352)		-1	2	2	37	31	-6	6	5	-1	
ductile,nMS (118)		1	1	0	22	22	0	4	4	0	
ductile,nMS,IP (86)		2	2	0	14	14	0	3	3	0	
brittle (37)		0	-1	0	17	17	0	4	4	0	
brittle, nMS(35)		-1	-1	0	17	17	0	4	4	0	
brittle,nMS,IP (29)		-2	-2	0	9	9	0	2	2	0	
extra-ductile (18)		2	2	0	12	12	0	3	3	0	
extra-ductile,nMS,IP	(16)	3	3	0	12	12	0	3	3	0	

# The divergence: Engineering vs Research

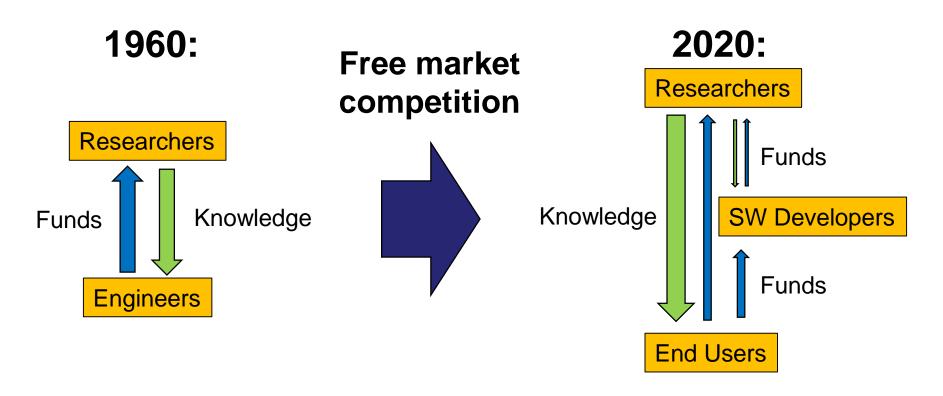
Real applications:	Methods Dang Van (1973) Findley (1957) McDiarmid (1991) Sines (1959) Matake (1977)	X Fe-Safe	X X MSC.Fatigue	K X FEARCE	X nCode DesignLife	K LMS Virtual. Lab Durability	X X WinLife	X X eFatigue		X X X PragTic	X FatLab		2.9- -0.1 -0.1 -0.2 -4.3 -4.3 -4.3		St. deviation of St. deviation of 12.2 12.2 12.2 12.2 12.2 12.2 12.2 12.	2 2 0 9
How they can live together?	Other solution Method:	C&S	Crossland	Dang Van	Findley	Fogue	Goncalves	L&M	T&Z		McDiarmid	Papadopoulos	Papuga PCr	Robert	Sines	Susmel
¢ ↑	Year of publication: Ref Year Sets Items	2001	1956	1973	1957	1987	2005	2005	1989	1977	1991 I	1994 Pa	2008 I	1988	1959	2001
Research:	Ref.         Year         Sets         Items           [8]         1997         4         43           [9]         1999         1         2           [10]         2000         ?         179           [11]         2001         3         30           [12]         2002         52         447           [13]         2003         3         38           [14]         2005         4         41           [15]         2006         1         8           [16]         2007         16         125	A	X X X X	X X X	X X		А		A X	X	X X X	X X X X X X X			Χ	А
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	$ \begin{bmatrix} 4 \\ 2011 & 49 & 407 \\ [21] & 2011 & 8 & 52 \\ [22] & 2013 & 8 & 62 \\ [23] & 2014 & 2 & 4 \\ [24] & 2014 & 18 & 58 \\ [25] & 2014 & 3 & ? \\ \end{bmatrix} $	X* A A	X* X* X X X	X* X*	X* X* X	X* X*	X* X* X	X*	X* X*	X* X*	X* X*	X* X* X	A*	X* X*	X* X* X X	X*
	[25]       2014       3       ?         [26]       2015       25       269         [27]       2015       7       26         Number of occurrences       Mean relative error [%]       5t. dev. of rel. error [%]	2 -4.8 8.7	13 -8.0 11.3	7 -0.1 12.2	X X 7 8.7 15.2	2 2.4 10.8	3 0.7 10.9	1 -1.2 12.1	3 0.0 8.8	X 7 6.4 15.8	7 -6.2	X 14 -4.6 10.3		2 4.7 9.9	X 7 -4.3 17.9	2 1.7 8.4

Commercial

Non-commercial

Test set 407 exps.

### Interaction of groups on market



"... The users don't really want to do their own research anymore. They expect nCode etc to "build-in" any new concept. Unfortunately this has stifled research by others. The major fatigue research labs in N.America are dying off. ..."

From personal e-mail communication with Al Conle (retired from Ford), 2009

# Fatigue solvers – Pros and Cons

#### ╋

- Computational power
- Ability to quickly iterate various design versions
- A "standardized" solution
- Stabilized quality of the output
- Cheaper than personnel costs
- No fear from leaves of crucial employees

- Dependence on knowledge generated and maintained out of house
- No idea how the solver really works
- Very limited possibility to improve solution, when it is obviously weak
- Warranty denial

	EUR	CZK	Reason		EUR	CZK	Reason
Year 1	30000	780000	Purchase	Year 6	7500	195000	Maintenance
Year 2	7500	195000	Maintenance	Year 7	7500	195000	Maintenance
Year 3	7500	195000	Maintenance	Year 8	7500	195000	Maintenance
Year 4	7500	195000	Maintenance	Year 9	7500	195000	Maintenance
Year 5	7500	195000	Maintenance	Year 10	7500	195000	Maintenance
Average/Year	12000	312000		Average/Year	9750	253500	
Average/Month	1000	26000		Average/Month	812.5	21125	

#### Warranty disclaimer issue

#### Researcher:

- Proposes a new criterion
- Proves its validity on limited data he has in hands
- His only (vague) responsibility is for these research results

#### Solver developer:

- Selects and implements the method
- I do not know about any case, where further testing was sponsored by such a company with publicly available results
- Decides to what extent to release publicly details of the implementation (so that the competitors would not steal his ideas)
- **Disclaims any responsibility** for the results of the software

#### End user - engineer:

- Gets a very expensive tool in his hands
- Due to high price is forced to use it to maximum
- Does not have time enough to get through all the theoretical basis or validation studies (if there are any available)
- Would like to believe that the previous two persons were responsible

#### Warranty denial vs Advertisement

 "MSC Fatigue enables durability engineers to quickly and accurately predict how long products will last under any combination of time-dependent or frequency-dependent loading conditions."

MSCsoftware.com (2018). MSC Fatigue: FE Based Durability Solution. [online] Available at: http://www.mscsoftware.com/product/msc-fatigue [Accessed August 30, 2018]

"Do I need to be a fatigue expert?"

No, you can leave that to us. There are factors which cannot be ignored if results are to be trusted. However, because fe-safe is technically advanced, it is configured to take into account many variables which will affect the accuracy of your results automatically."

3ds.com. (2018). FE-SAFE - SIMULIATM 3D Software - Dassault Systèmes®.
[online] Available at: https://www.3ds.com/productsservices/simulia/products/fe-safe/ [Accessed August 30, 2018].

# Why it went this way?

- Computerized society
- Cost cuts: Own research is too expensive and unpredictable
- Increased complexity of computational models
- Humans from the perspective of managers:
  - Unreliable
  - Expensive
  - Hard to raise
  - Unstable: Prone to leave if not well kept

**The goal today - Search for an intelligent system:** The same (wo)man builds the virtual CAD model, meshes it, adds boundary conditions and runs the FE-analysis, which (s)he then uses for the subsequent fatigue analysis. The computer (program) assists to these actions and prevents any potential errors.

# Reminder: Engineering vs Research

How they can live together?

Real applications:

Research:

Is the free market self-correcting?

Yes, it would be, if there had been somebody responsible

			Comm	ercial			1	Non-o	comme	ercial		Test set 407 exps.			
Methods	X Fe-Safe	K MSC.Fatigue	Femtat FEARCE	nCode DesignLife	LMS Virtual. Lab Durability	WinLife	X eFatieue	X Code Aster	X PragTic	FatLab		Mean relative	error [%]	St. deviation of relative error	[%]
Dang Van (1973)	X	X	x	X	X	Х						-0.	1	12.2	2
Findley (1957) McDiarmid (1991)		х	х	х		Х	Х		X X	Х		8.7 -6.2		15.2 12.0	
Sines (1959)							Х		Х			-4.	3	17.9	
Matake (1977) Other solution		3	x					X X		Х		6.4	ŀ	15.8	8
											SC	5			
	S	land	Dang Van	lley	ang	Goncalves	M	Ŋ	ake	McDiarmid	1994 Papadopoulos	Papuga PCr	ert	es	nel
Method:	C&S	Crossland	Dang	Findley	Fogue	Bonc	L&M	L&Z	Matake	[cDi	pado	apug	Robert	Sines	Susmel
	_			6	5		10	~	~		t Paj		~	~	_
Year of publication:	2001	1956	1973	1957	1987	2005	2005	1989	1977	1991	$199_{2}$	2008	1988	1959	2001
Ref Year Sets Items [8] 1997 4 43	;	X							X	X	X			X	
[8] 1997 4 43 [9] 1999 1 2		X	х						Α	Λ				А	
[10] 2000 ? 179 [11] 2001 3 30	А			х				А	х	х	Х				
[12] 2002 52 447											Х				А
[13] 2003 3 38 [14] 2005 4 41		X X	х			А					X X				
[15] 2006 1 8 [16] 2007 16 125	х		Х	Х				Х		x	Х				
[17] 2008 4 43	$\mathbf{\Lambda}$	Х							Х	-	Х				
[18] 2009 40 320 [19] 2010 13 131		X X	х						Х		X X	Х			х
[20] 2010 6 66	77₩	$\mathbf{X} \mathbf{X} \mathbf{X}^*$	X*	X*	X*	X*	X*	X*	X*	X X*	X*	A*	X*	X X*	X*
[21] 2011 8 52	X* A	$X^*$	$X^*$ $X^*$	$X^{*}$ $X^{*}$	$X^*$ X*	$X^*$ X*	$\Lambda^{\tau}$	$X^*$ X*	$X^*$ $X^*$	$X^*$ $X^*$	$X^*$ X*	$\Lambda^{+}$	$X^{*}$	$X^*$	$\Lambda^{\pi}$
[22] 2013 8 62 [23] 2014 2 4		X X		х										X X	
[24] 2014 18 58	А	X				Х					Х				
[25] 2014 3 ? [26] 2015 25 269			Х	X X						Х	х			Х	
[27] 2015 7 26	2	13	7	7	2	3	1	3	X 7	7	X 14	1	2	7	2
Number of occurrences Mean relative error [%]	-4.8	13 -8.0	-0.1	8.7	2 2.4	3 0.7	1 -1.2	0.0	6.4	-6.2	-4.6	1 -0.5	2 4.7	-4.3	2 1.7
St. dev. of rel. error [%]	8.7	11.3	12.2	15.2	10.8	10.9	12.1	8.8	15.8	12.0	10.3	6.1	9.9	17.9	8.4

#### Market doesn't favor the best but the cheapest

- 1. Engineering companies wanted to cut their costs for fatigue analyses.
- 2. They started to buy fatigue solvers, which can be developed cheaply, without the need to support own research.
- 3. The money paid for fatigue solvers enabled developers to develop solvers, but there was little real research underlying them.
- 4. Solver developers became aware that they cannot substitute research, so they avoided providing a warranty.
- Academia lost interest in what was implemented in fatigue solvers (no more money, no research).
- Nobody has been taking care of the core methods in fatigue solvers. They are generally considered or assumed to be good enough (whatever this means).

#### The outcome?

#### 1. Researchers

- The big losers no gain anywhere
- They have lost the funding for research to confirm or reject the implemented methods, to publish results, and to create and publish benchmarks.

#### 2. End users

- Win on the level of their company (savings on investment)
- They have lost control over potential prediction quality.

#### 3. Solver developers

- The only current winners (money from their customers).
- In the long-term, however, they are doomed to lose their credibility, unless they start to re-invest into research.
- The only relevant customers for them are the bigger customers, who are able to do their own benchmarking.

### **Room for Verification Authority**

- To bridge the gap between research and commercial application
- Need for verification of
  - methods implemented in SW
  - the implementation ways themselves
  - new calculation methods where a great potential of commercial implementation exists

### NAFEMS case

"By the late 1970's and early 1980's, as computing power became more widely available, increasingly industry was starting to solve practical engineering problems using finite element analysis techniques.

There was however considerable concern that the accuracy of the methods, and software implementations, required to be verified in order to allow the results to be effectively used."

from: http://www.nafems.org/about/about\_nafems/history/

- NAFEMS (National Agency for Finite Element Methods and Standards) established in 1983 "To promote the safe and reliable use of finite element and related technology"
- Funded for 7 years by UK government
- Then switched to a non-profit organization funded by its activities and members
- Shift in the focus
  - Originally Benchmarks to test the FE-solvers
  - Now Continuous education of FE-analysts

 "Except as specifically permitted in this Agreement, Customer agrees not to: (a) ... (e) provide, disclose or transmit any results of tests or benchmarks related to any DS Offering to any third party,..."
 DASSAULT SYSTEMES. (2018). Customer License and online service agreement. [v. 11.2], DASSAULT SYSTEMES.

 This means, that every customer is left alone, without any legal chance to understand better the offer on the market

# Why this could happen?

#### Engineers

- Love complex technical systems
- They are happy somebody / something pretends to remove their responsibility

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 They are not demanding the responsibility of others

#### FADOFF -> Fatigue Limit (Dummy Model)

- New solution prepared within FADOFF
- APDL script in ANSYS to prepare a single fictitious (dummy) model, where on elements and nodes are
  - predefined material properties
  - history of stress tensor components

- 325 experimental items now
- **Effect:** 
  - Any user of a commercial fatigue solver can
    - use it as an input for preparing fatigue prediction
    - solve it by the methods implemented in his fatigue solver
    - check the prediction capability of his fatigue solver

#### Some output...

Two
commercial
fatigue solvers
(CFS) available
for testing

Two more could be checked this year

CFS#1 (Dang Van)

	N of		avera	ge ∆FI		st	andard dev	viation of $\Delta$	\FI
Group	items	CFS#1	CFS#2	PragTic	PragTic	CFS#1	CFS#2	PragTic	PragTic
	items	Dang Van	Dang Van Optimum F		Dang Van	Dang Van	Optimum	PCR	Dang Va
All	325	-13.2%	-0.5%	1.6%	-2.9%	30.6%	15.3%	7.6%	17.19
MS	190	-17.4%	-0.6%	1.4%	-5.5%	32.9%	17.4%	7.9%	19.9
nMS	133	-7.6%	-0.6%	1.9%	0.8%	26.1%	11.9%	7.2%	11.19
Sync	72	-18.0%	-1.9%	2.9%	-3.6%	34.2%	13.9%	8.9%	17.6
brittle	38	-0.7%	2.5%	3.7%	2.5%	26.6%	16.3%	8.2%	21.6
brit,nMS	23	-0.7%	-1.0%	1.4%	0.9%	14.5%	14.4%	6.5%	13.1
ex-duct	45	-28.7%	3.4%	-3.7%	-16.5%	31.9%	22.9%	9.1%	15.8
AT	219	-14.2%	-2.6%	2.1%	-3.1%	30.1%	13.0%	8.0%	14.5
2-3A	39	6.9%	-7.0%	2.3%	11.2%	15.2%	15.3%	7.4%	16.4
IP	112	-5.4%	2.6%	1.6%	1.2%	25.3%	8.9%	6.5%	12.3
IP,nMS	100	-2.0%	3.4%	2.6%	3.7%	22.1%	8.2%	5.7%	8.2
IP,nMS,s	57	-2.2%	3.0%	2.5%	3.4%	23.2%	9.5%	6.1%	9.4
IP,nMS,t	43	0.3%	3.5%	2.5%	3.7%	15.5%	6.2%	5.3%	6.2
MS,Ax	43	-21.0%	8.6%	1.0%	-6.3%	38.8%	16.9%	4.8%	21.6
MS,To	23	-25.4%	12.6%	-2.4%	-19.1%	21.1%	17.6%	7.3%	13.0
OP	82	-14.1%	-13.0%	0.7%	-4.5%	27.8%	12.6%	9.1%	19.2
OP,nMS	31	-21.5%	-14.4%	-0.3%	-9.8%	24.7%	11.5%	10.7%	12.9
OP90,nMS	23	-23.8%	-18.0%	-1.1%	-12.6%	22.3%	10.3%	11.8%	13.0
OP,MS	52	-9.9%	-12.0%	1.6%	-1.5%	28.5%	13.1%	8.2%	21.3
OP,MS,AT	27	-27.3%	-10.3%	2.8%	-15.6%	27.9%	14.6%	9.9%	16.2

- ¾ of results agree very well with PragTic (Dang Van), the rest does not
- no similar markers for failure, results tend to be too unsafe
- Was communicated to the developer No interest!

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